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Development of a Heat Recovery unit for Residential Applications

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Abstract

When considering the design for a heat recovery unit for residential applications, there are many possible configurations. The most fundamental design will be some form of heat exchanger that will use hot air to heat a cool fluid stream of water. The task is to design a unit for heating water flowing at 2.12 LPM by exactly 4 degrees centigrade from an initial temperature between 22.0and 24.0. Any deviations in this temperature change must be justified. The heat exchanger used for preliminary calculations is an unfinned counter flow heat exchanger; however, different con figurations will be explored throughout this report to determine the most efficient one with the smallest area of heat transfer.

The overall design of the unit has very few constraints, and any reasonable model can be considered. The only given design constraint is that the air or hot fluid must have an outlet diameter of 6 inches, and the warm air flow must exit at a velocity of 10 m/s and a temperature of 45 degrees centigrade. Some fair assumptions that were made are that the thermal properties will remain consistent, both fluid streams are fully developed, the kinetic and potential energy changes are negligible, and that no heat is lost to the surroundings. The preliminary design resulted in about 16% efficiency. For the initial calculations, the inlet and outlet diameter will be the same and any potential fouling factors will be ignored. The fouling factor, however, will be considered in later designs.

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I. Introduction

For this report, a heat recovery unit for residential application was used to design and analyze aheat exchanger. Devices like heat exchangers are used since they facilitate the exchange of heatbetween fluids having different temperatures without having to mix them, unlike mixingchambers where the fluids do mix. To analyze the heat transfer between the fluids, the overallheat transfer coefficient, U, is used, taking into account all the effects during heat transfer suchas convection and conduction. Heat transferred from the hot fluid to the wall is done byconvection through the wall by conduction and again by convection from the wall to the coldfluid. Thermal resistance through a tube wall can be negligible when the wall thickness of thetubes is small as it is in this case. With a quick literature search, numerous articles point out theuse of a heat recovery unit when looking at history; it is unclear when it was first invented.

Nevertheless, there are patents dating from 1983 by Rolf A. S. Kruse, Karl A. L. Gustavsson, Karl A. Jansson. At first glance, it may seem obsolete, but the critical function is recovering theheat. It is essential to look back on patents to know which path to follow or solely for inspiration.

Furthermore, Heat recovery units are tremendously beneficial as they help recover most of theheat that is typically wasted and reduce heating requirements. This closed-cycle improves efficiency when compared to old methods. heat recovery circulates fresh air А unit hot in ourhomes; it also keeps out moisture and pollutants. Moisture and contaminants are created by things simple as as breathing and cooking. If humidity reaches excessive levels, it can causestructural damage. Our heat exchanger is a subunit of a complex architecture, but the generalpurpose is to heat fresh air without going stale. There are several different makes and models, butmost heat recovery units will gain back 80%-85% of the heat of the existing stream. They can beused in an independent heat recovery unit installation or a heat recovery with a furnace. Thesecond option is when our heat exchanger comes into play, replacing the furnace.

In this project, a heat exchanger is installed in the exhaust of the heat recovery unit, where thehot exhaust air will be utilized to heat cold water. A heat exchanger is to be designed andanalyzed to acquire the goal of warming the cold water 4C. Analytical and modeling methodswere applied using Fusion 360, and ANSYS. Designs were replicated in NX-10, but it wasincompatible with ANSYS. The heat exchanger design was done using Fusion 360 and wasimported to ANSYS to perform simulation and analyze results acquired and compare to theanalytical results. This project aims to demonstrate the application of a counterflow heatexchanger using analytical calculations and CFD software to validate our design. The finalmodel should be capable of heating water by 4 Celsius.

Theoretical Background

Heat recovery units come in different types of forms depending on what the unit needs to be usedfor, but they all contain a type of heat exchanger for it to be operable. When using heat recoveryunits for residential, it is important to be set up in the most convenient area. Heat recoverysystems are used for heat spaces, ventilating spaces, heating water, and industrial scale drying.

The way these types of systems work is hot fluid passes next to cold fluid and the heat transferson to the colder fluid hence the name heat exchanger. When putting a heat recovery unit in ahome or office, heat recovery units work just like a ventilation system where it involves a type ofheat exchanger that can sit on the roof, where it draws the cold air from the outside and warms itup with air that is being expelled from the inside.

It is known that a heat exchanger is the brain of a heat recovery unit. The role of heat exchangersis to cool or heat fluids in a system. When creating a heat exchanger for an application a lot ofproperties of the heat exchangers be taken into consideration from the fluid being must used. sizeofpipes.towhattypeoffittingsandwhattypeofmaterialwillbeusedforthepipingaswellasif it will have fins or not. When creating a heat recovery unit for a residential application having an efficient heat exchanger in the system is needed to work properly.

There are two types of heat exchangers that are mostly used in different types of systems thatoperate very differently based on the direction of the flow of the fluid. The two types of heatexchangers that are the most common are parallel flow and counter flow, and for the heatrecovery unit it was decided that a counter-flow heat exchanger would be the best type of heatexchanger to use. The counter-flow heat exchanger works by having a stream of one of the fluids in the opposite direction of the flow of the other fluid compared to the parallel where the fluidflows in the same direction. Since counter flow heat exchangers have the hot fluid going throughone side and the hot fluid through the other, it is more efficient because it minimizes the thermalstresses through the exchanger has largetemperature differences atthe endswhich causes large thermal stresses. When creating a heat exchanger an important property iscross flow whether it is un-finned or finned. When a heat exchanger is finned tubular both fluidsare unmixed, and fins are guided in a direction transverse to the tube flow direction. When theheat exchanger is un-finned heat can be exchanged in all directions so that there's a chance that the fluid can mix.

Analytical Calculations

| Properties of Air | Temp (C) | Density (kg/m^3) | Specific Heat (J/kg*K) | Thermal Conductivy (W/m*K) | Dynamic Viscosity (kg/m*s) | Prandtl Number |
|---------------------|-------------|------------------|------------------------|----------------------------|----------------------------|----------------|
| Air in | 45 | 1.109 | 1007 | 0.02699 | 0.00001941 | 0.7241 |
| Air Out | 42.10895909 | 1.1198 | 1007 | 0.0268 | 0.000019272 | 0.7249 |
| Air film | 43.55447955 | 1.1144 | 1007 | 0.0269 | 0.000019341 | 0.7245 |
| | | X450 | | | | |
| Properties of water | Temp (C) | Density (kg/m^3) | Specific Heat (J/kg*K) | Thermal Conductivy (W/m*K) | Dynamic Viscosity (kg/m*s) | Prandtl Number |
| Water in | 23 | 997.4 | 4180.8 | 0.6034 | 0.0009354 | 6.488 |
| Water out | 27 | 996.6 | 4179.2 | 0.6102 | 0.0008538 | 5.852 |
| Water avg | 25 | 997 | 4180 | 0.607 | 0.000891 | 6.14 |

Table 1: Water and Air Properties

Calculating volume flow rate for water $V=(2.12LPM)(\frac{1minute}{60seconds})(\frac{1m^{3}1}{000L})=0.00003533m^{3}/s$ Calculating for mass flow rate $m_{water} = \rho * volume flow rate = (997kg/m^{3})(0.00003533m^{3}/s)=0.03522401 kg/sec$

 $m_{air} = \rho * velocity * Ac = (1.109 kg/m^3)(10m/s)((\pi/4)(0.1524m)) = 0.20229879 kg/s$

Calculating for volume flow rate of air

 $V = \frac{\rho}{massflowrate} = \frac{1.109 kg/m^3}{0.20229879 kg/s} = 0.1824146925 m^3/s$

Heat Transfer

 $\begin{aligned} & Cc(water) = massflowrate * Cp = (0.03522401 kg/sec)(4180J/kg * K) &= 147.2363618 W/K \\ & Cc(air) = massflowrate * Cp &= (0.20229879 kg/s)(100 el7J/kg * K) = 203.7139792 W/K \\ & Cmin = Cc(water) = 147.2363618 W/KCr = 203.7139792 W/K \\ & Cc(water) = 147.2363618 W/KCr = 203.7139792 W/K \\ & Cc(water) = 147.2363618 W/KCr = 203.7139792 W/K \\ & Cc(water) = 147.2363618 W/KCr = 203.7139792 W/K \\ & Cc(water) = 147.2363618 W/KCr \\ & Cc(water) = 147.2367618 W/KCr \\ & Cc(water) = 147.2367618 W/KCr \\ & Cc(water) = 147.236$

Cmin/Cmax = 0.7227602267

 $Q_{max} = Cmin(Thot, in - Tcold, in = (147.2363618W/K)(45^{\circ}C - 23 = 3239.19996W)$

Effectiveness

$$\epsilon = Q/Q_{max}(100) = 18.1818\%$$

NTU $NTU=\frac{1}{c-1}ln(\frac{c-1}{cc-1})=.2156455726$

Reynolds Number

$$\begin{split} Re_{water} = & \frac{4*massflowrate}{\pi Di\mu} = 5355.94082(Turbulent) \\ Re_{air} = & 87385.14038(Turbulent) \end{split}$$

Nusselt Number

Using Table 7-1 from Heat and Mass Transfer Fundamentals and analyzing the range of Reynolds number for water, the equation used for Nusselt number is the following:

 $Nu_{water} = 0.193 Re^{0.466} Pr^{1/3} = 5355.94082$ $Nu_{air} = 0.023 Re^{0.8} Pr^{0.3} = 215.9769787$

Heat transfer Coefficient

Using the Nusselt number equation to solve for h,

$$\operatorname{Nu}_{Cyl} = \frac{hD}{k}$$
 : h = $\frac{Nu_{Cyl}kD}{k}$

h_{water}=4601.017186*W*/m2*Kh_{air} =38.12192077*W*/m2*K

Overall heat transfer coefficient $\mathcal{U} = \underbrace{1}_{h_{atr}^+ h_{water}} = 37.80865557 \text{W/m}^{2*} \text{K}$

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LMTD

 $\Delta T1 = Thot, in-Tcold, out = 18^{\circ}C \\ \Delta T2 = Thot, out-Tcold, in=19.10895909^{\circ}C$

$$TLM = \frac{\Delta T1 - \Delta T2}{ln(\Delta T/\Delta T2)} = 18.5489549$$

Surface Area

Using the equation for heat transfer to solve for the surface area

$$Q=UAs\Delta Tlm$$
 \therefore $As= \frac{Q}{U*\Delta Tlm} = 0.8397777986m$

Modeling Set Up

The heat exchanger was designed using Fusion 360 and was later imported into ANSYS toperform the simulation. As settings were modified during the setup process, many results anderrors were obtained. Multiple heat exchanger designs were attempted to achieve a temperature difference of 4 degrees celsius. The one below was the closest to achieving the 4 degrees. The different heat exchangers can be found in the appendix section of this report.



Figure1. Applying mesh to outer fluid

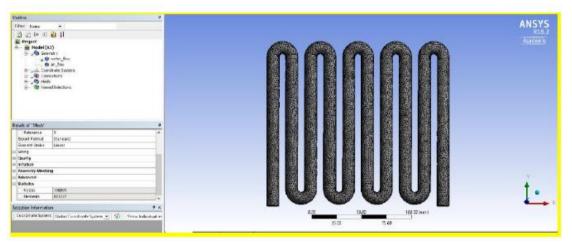


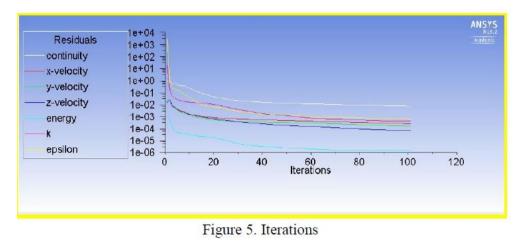
Figure 2. Applying mesh to copper pipes and inner fluid

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Figure 3. Simulation Conditions

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Figure 4. Running Calculations



II. Results

ANSYS simulation was performed on three different CAD models with three different numbers passes (17, 11, and 10). There were technical limitations on geometry and design whensimulating ANSYS, which made our initial theoretical design impossible to simulate on thesoftware. The following results are the velocity, pressure, and temperature contours retrieved from simulating the 10 tubbed CAD design, which represents the most accurate simulation whencompared to our analytical calculations.

Velocity Contour:

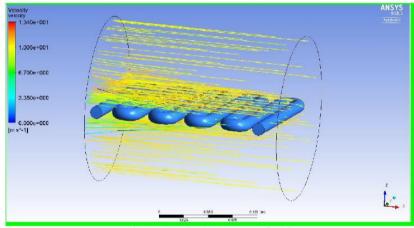


Figure 6. Velocity Contour (m/s)

Computational Fluid Dynamics (CFD) simulations were carried out to simulate the air flowthrough the test subject. We know that the performance of the heat exchanger is greatly affected by the distribution of air that passes through it and the features within the duct and theorientation of the heat exchanger.

Simulation shows air flowing inside the heat exchanger in a range between 0 m/s and 13.1 m/s, which agrees with the 10 m/s initial velocity declared in the set up.

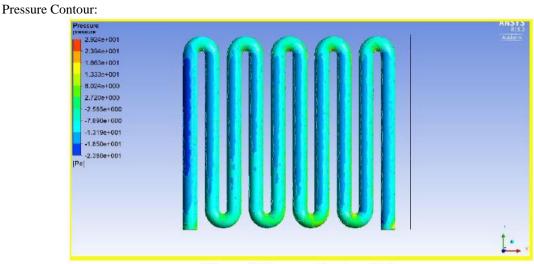


Figure 7. Pressure Contour (Pa)

The pressure contour obtained from ANSYS confirms that pressure does not remain constant inheat exchangers. This can be attributed to the fact that the fluid flowing inside the tube willcreate friction that leads to unavoidable pressure drop. Our simulation shows a range in pressurebetween -23.8 Pa and 29.2 Pa.

Temperature Contour:

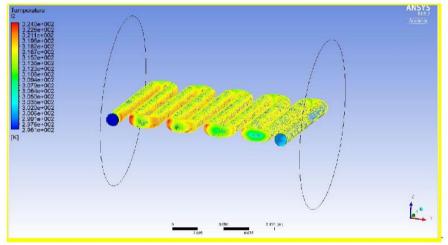


Figure 8. Temperature Contour (K)

The temperature contour shows a minimum temperature of 296.1 K located at the water inlet of the pipe. The water outlet shows a temperature in a blue gradient, which can be estimated to be between 299 K and 300 K, proving that this design successfully heats water by 4 degrees.

Costs

| | | # of Days | # of Hrs | Price S/kWhr | Q Air kW | Cost per Month | Cost per Seasor |
|-----------------|-----------|-----------|----------|--------------|----------|----------------|-----------------|
| | January | 31 | 744 | 0.1111 | 0.588 | 48.6031392 | Winter |
| | February | 28 | 672 | 0.1111 | 0.588 | 43.8996096 | 141.105888 |
| | March | 31 | 744 | 0.1111 | 0.588 | 48.6031392 | Spring |
| | April | 30 | 720 | 0.1111 | 0.588 | 47.035296 | 149.0975136 |
| | May | 31 | 744 | 0.1222 | 0.588 | 53.4590784 | Summer |
| | June | 30 | 720 | 0.1222 | 0.588 | 51.734592 | 158.6527488 |
| | July | 31 | 744 | 0.1222 | 0.588 | 53.4590784 | Fall |
| | August | 31 | 744 | 0.1222 | 0.588 | 53.4590784 | 152.2289664 |
| | September | 30 | 720 | 0.1222 | 0.588 | 51.734592 | |
| | October | 31 | 744 | 0.1222 | 0.588 | 53.4590784 | |
| | November | 30 | 720 | 0.1111 | 0.588 | 47.035298 | |
| | December | 31 | 744 | 0.1111 | 0.588 | 48.6031392 | |
| Total in 1 Year | | 365 | 8760 | | | 601.0851168 | |

Figure 9. Cost of One Year

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| Inflation Ove | ar 10 Years |
|---------------|-------------|
| 2020 | \$601 |
| 2021 | \$616 |
| 2022 | \$631 |
| 2023 | \$647 |
| 2024 | \$663 |
| 2025 | \$680 |
| 2026 | \$697 |
| 2027 | \$714 |
| 2028 | \$732 |
| 2029 | \$751 |
| 2030 | \$769 |
| Total Cost | \$7,501 |

Figure 10. Total Life Cycle Cost

| Materials and Equip | ment | | |
|--|---------------|-------------|-------------|
| Item | Amount Needed | Price | Total Price |
| Copper Tubing 3/8 Tube Size, 1/2" 0D.0.065" Wall Thickness | 78" | \$33.61-6ft | \$50.41 |
| Mulipurpose Copper Sheet, .002" thick, 2" X 50 ft | 1 Unit | \$42.23 | \$42.23 |
| 304 Stainless Steel Pipe, 6.625 0D X.280 wall X 6.065 ID | 1 Unit | 369.06-2ft | \$369.06 |
| Starbond Super Fast Thin CA Glue EM-02 | 1 Unit | \$10.50 | \$10.50 |
| έ | 8) | Total= | \$472.20 |

Figure 11. Initial Costs

The total cost was calculated using the residential electricity rates in El Paso. To get the monthlycost, Qair was multiplied with the hours of the month, and then multiplied by the rate. The average costs during the summer months are 12.22 ¢/kWhr and in the winter it is 11.11 ¢/kWhr. To calculate the costs over a span of 10 years, inflation was taken into consideration. In the final report, maintenance costs will also be included

Safety Considerations

Heat exchangers are essential equipmentfor a manufacturing plant. However, heat exchangersoperation and maintenance contain potential safety hazards to prevent any accidents, even death.Safety is a crucial part of the design and building to prevent accidents and also life cost of theheat exchanger.According to frankieidson.com, an injury lawyer, "Every year in the US .,power tool injuries result in approximately 400,00 emergency rooms visits". Toreduce the risksof getting hurt the adequate personal protective equipment (PPE) should be used by every teammember. Safety goggles protect the eyes from residue from pipes being cut,helmets as well toget protection from flying objects ,gloves to protect hands from hot surfaces and sharp objects. Itis also imperative to always be a supervisor in case of accidents and never operate a machine orheat exchanger by yourself.

III. Conclusion

In this project, a heat recovery unit was created and simulated for the purpose of heating water4°C. Waterand air entered the heat recovery unit at 23°C and45°C respectively. All initialproperties were collected at those temperatures to help calculate both mass flow rates. Once thatwas calculated, the heat transfer, effectiveness, and NTU were calculated. The NTUwas used todetermine the Reynolds and Nusselt number. The heat transfer coefficient and LMTD were thencalculated to find the surface area. Multiple heat exchangers of different sizes were created to get aheat increase of 4°C. The final CAD design consisted of ten tubes and nine 180- elbows. Thisspecific heat exchanger size was the one that yielded the closest increase to 4°C. However, thefinal temperature at the water outlet is 27.3C. The reason for not getting exactly 4C could've been caused for numerous reasons including mesh size, number of iterations, and quality.

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